

## Research Article

# Amplitude Modulation and Synchronization of Fractional-Order Memristor-Based Chua's Circuit

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This paper presents a general synchronization technique and an amplitude modulation of chaotic generators. Conventional synchronization and antisynchronization are considered a very narrow subset from the proposed technique where the scale between the output response and the input response can be controlled via control functions and this scale may be either constant (positive, negative) or time dependent. The concept of the proposed technique is based on the nonlinear control theory and Lyapunov stability theory. The nonlinear controller is designed to ensure the stability and convergence of the proposed synchronization scheme. This technique is applied on the synchronization of two identical fractional-order Chua's circuit systems with memristor. Different examples are studied numerically with different system parameters, different orders, and with five alternative cases where the scaling functions are chosen to be positive/negative and constant/dynamic which covers all possible cases from conventional synchronization to the amplitude modulation cases to validate the proposed concept.

## 1. Introduction

Despite that the history of fractional calculus started in the same period of time as integer calculus, the major revolutions in this area have been discovered only during the last five decades where the realization, modeling, and numerical simulations were available [1–4]. Similarly, the chaotic systems have been studied heavily during the last four decades since they play an important role in industrial applications particularly in chemical reactions [5], biological systems [6], circuit theory [7–11], control [12], and security applications [13–16]. Recently much attention has been devoted to the search for better and more efficient methods for the control or determination of a solution, approximate or analytical, of chaotic systems.

Antisynchronization is a phenomenon in which the state vectors of the synchronized systems have the same amplitude but opposite signs to those of the driving system. Therefore, the sum of two signals is expected to converge to zero when antisynchronization appears. Since the discovery of

antisynchronization experimentally in the context of self-synchronization, it has been applied in many different fields, such as biological and physical systems, structural engineering, and ecological models [17]. Liu et al. [18] show that either synchronization or antisynchronization can appear depending on the initial conditions of the coupled pendula. Active control method is used to study the antisynchronization for two identical and nonidentical systems [19–21].

The synchronization of fractional chaotic systems has started to attract much attention and has also raised up some problems [22–24]. Recently the consistency of the improvement of models based on fractional-order differential structure has increased in reputation in the research of dynamical systems [25–27]. Yu et al. studied the synchronization of three chaotic fractional-order Lorenz systems with bidirectional coupling [28], Odibat et al. [29] investigated the chaos synchronization of two identical systems via linear control, and Bhalekar and Daftardar-Gejji [30] demonstrated that two different fractional-order chaotic systems can be synchronized using active control.

Recently, Radwan et al. [31] developed a framework to obtain approximate numerical solutions of the fractional-order Chua's circuit with memristor using a nonstandard finite difference method. The most important advantage of using fractional order is to increase the chaotic range as proven from the stability analyses of this circuit in both the W-plane and s-plane. Moreover, another circuit from Chua's family was studied and modified with the use of memristor with detailed responses by Petráš in [32]. In this paper, the concept of dynamic scaling between the master and slave systems in the fractional-order domain is introduced. The proposed concept covers the conventional synchronization up to the amplitude modulation technique. Different examples have been studied based on the nonlinear antisynchronization of two identical fractional-order chaotic Chua's circuits with memristor. This generalized projective synchronization is based on the nonlinear control theory and Lyapunov stability theory.

The paper is organized as follows. In Section 2 we provide some mathematical models of the fractional calculus theory and describe the nonstandard finite difference scheme to solve fractional differential equations and in the last subsection we present the fractional Chua's circuit with memristor. Nonlinear antisynchronization of two identical fractional-order chaotic Chua's circuit systems is also introduced in Section 3, while the generalized projective synchronization is discussed in Section 4. Finally, conclusions are drawn in the last section.

## 2. Fractional Order System Memristor Based Chua's Circuit

Recently, most of the dynamical systems based on the integer-order calculus have been modified into the fractional order domain due to the extra degrees of freedom which increase the flexibility of the design and can be used to precisely fit the experimental data much better than the integer-order modeling. The Caputo fractional derivative of order  $\alpha$  of a continuous function  $f: R^+ \rightarrow R$  is defined as follows:

$$\begin{aligned} D^\alpha f(t) &\equiv \frac{d^\alpha f(t)}{dt^\alpha} \\ &= \begin{cases} \frac{1}{\Gamma(m-\alpha)} \int_0^t \frac{f^{(m)}(\tau)}{(t-\tau)^{\alpha-m+1}} d\tau, & m-1 < \alpha < m, \\ \frac{d^m}{dt^m} f(t), & \alpha = m, \end{cases} \end{aligned} \quad (1)$$

where  $m$  is the first integer greater than  $\alpha$  and  $\Gamma(\cdot)$  is the gamma function and is defined by

$$\Gamma(z) = \int_0^\infty e^{-t} t^{z-1} dt, \quad \Gamma(z+1) = z\Gamma(z). \quad (2)$$

The Grünwald-Letnikov method of approximation for the one-dimensional fractional derivative is as follows [33]:

$$D^\alpha x(t) = f(t, x), \quad (3a)$$

$$D^\alpha x(t) = \lim_{h \rightarrow 0} h^{-\alpha} \sum_{j=0}^{t/h} (-1)^j \binom{\alpha}{j} x(t-jh), \quad (3b)$$

where  $\alpha > 0$  and  $D^\alpha$  denotes the fractional derivative. Also  $N = [t/h]$ , and  $h$  is the step size. Therefore, (3a) and (3b) is discretized as follows:

$$\sum_{j=0}^{n+1} c_j^\alpha x(t-jh) = f(t_n, x(t_n)), \quad n = 1, 2, 3, \dots, \quad (4)$$

where  $t_n = nh$  and  $c_j^\alpha$  are the Grünwald-Letnikov coefficients defined as

$$\begin{aligned} c_j^\alpha &= \left(1 - \frac{1+\alpha}{j}\right) c_{j-1}^\alpha, \\ c_0^\alpha &= h^{-\alpha}, \quad j = 1, 2, 3, \dots \end{aligned} \quad (5)$$

The nonstandard discretization technique [34] is a general scheme where we replace the step size  $h$  by a function  $\varphi(h)$ . By applying this technique and using the Grünwald-Letnikov discretization method [2, 31], it yields the following relations:

$$x_{n+1} = \frac{-\sum_{j=1}^{n+1} c_j^\alpha x_{n+1-j} + f_1(t_{n+1}, x_{n+1})}{c_0^{\alpha_1}}, \quad (6)$$

where  $c_0^{\alpha_1} = (\varphi_1(h))^{-1}$  are functions of the step size  $h = \Delta t$ , with  $\varphi_1(h) = h + O(h^2)$ , when  $h \rightarrow 0$ . The fractional-order Chua's circuit [31] based on the new nanodevice element which is called memristor [35–38] is shown in Figure 1 with its  $q-\phi$  relationship. The canonical memristor-based fractional-order Chua's circuit can be written as follows:

$$\begin{pmatrix} D^\alpha x \\ D^\beta y \\ D^\gamma z \\ Du \end{pmatrix} = \begin{pmatrix} -ak & a & 0 & 0 \\ -1 & 0 & 1 & 0 \\ 0 & -b & c & 0 \\ 1 & 0 & 0 & 0 \end{pmatrix} \begin{pmatrix} x \\ y \\ z \\ u \end{pmatrix}, \quad (7a)$$

$$k = \begin{cases} m_1 & |u| < 1, \\ m_2 & |u| > 1, \end{cases} \quad (7b)$$

where  $a, b, c, m_1$ , and  $m_2$  are related to the circuit parameters [31]. The effect of the memristive property appears through the parameter  $k$  (the slope of the charge with respect to the flux in the memristor) which is a piecewise-linear function with two different slopes  $m_1$  and  $m_2$  depending on the value of the flux  $u$  (Figure 1(b)). It is clear that the system has four variables which are  $\{x, y, z$ , and  $u\}$  and the chaotic behavior exists in a wider range as proved in [31]. The chaotic behavior has been verified by the calculation of the maximum

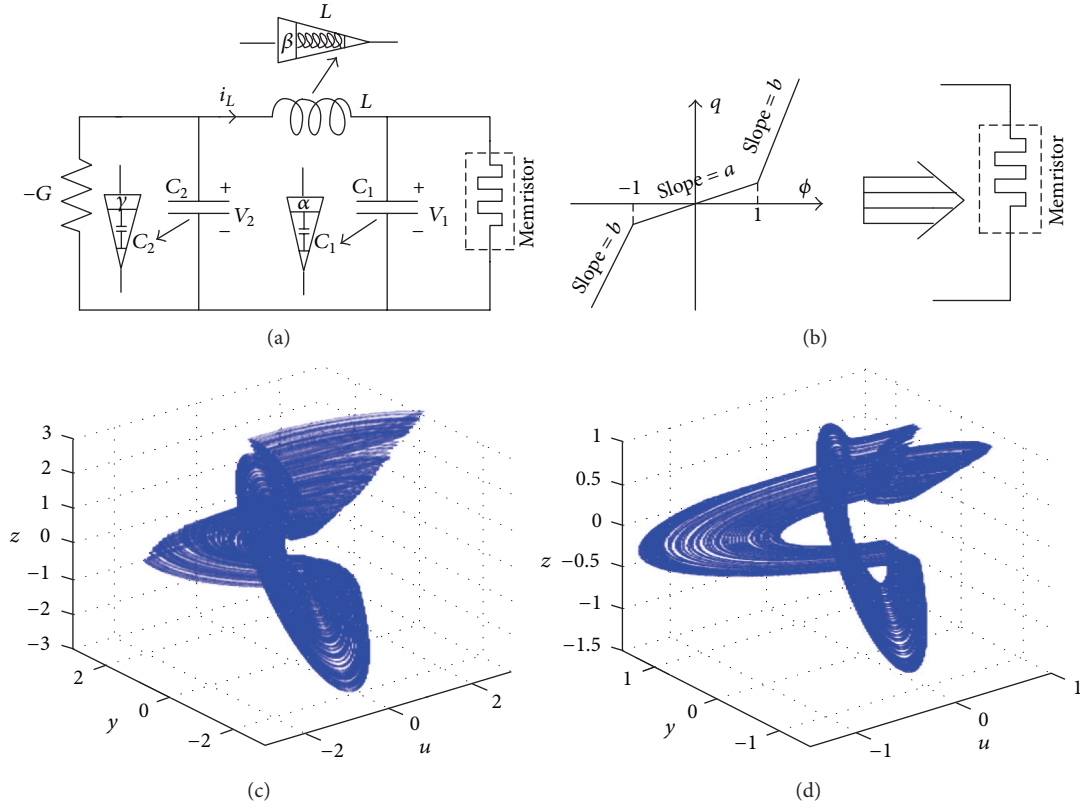


FIGURE 1: (a) The canonical Chua's circuit with memristor, (b) the piecewise-linear flux-controlled memristor, and (c) 3D shapes in the  $u$ - $y$ - $z$  plane when  $(\alpha, \beta, \gamma)$  (a) (1.0, 0.9, 0.9) and (d) (1.1, 0.9, 0.9).

Lyapunov exponent (MLE). Figures 1(c) and 1(d) show the chaotic responses for two different cases where the  $\alpha$  order changes from 1.0 to 1.1. It is clear from these subfigures that the output response is very sensitive to the fractional-order parameters. Therefore, these fractional-order parameters can be used for extra degrees of freedom and also to control the behavior of the strange attractors of the Chua's circuit.

### 3. The Proposed Technique

From the previous section, the fractional-order memristor-based Chua's circuit has ten parameters which are three fractional-orders  $\{\alpha, \beta, \gamma\}$ , three system parameters  $\{a, b, c\}$ , and the initial conditions. Figure 2 shows the general block diagram of the proposed system assuming that the fractional-orders of the two systems are identical but the other seven parameters may be different. The idea is based on modifying the equations of the second system by adding control functions  $\{u_1, u_2, u_3, u_4\}$  on the four equations to minimize the functions  $x_1 + s_1 x_2$ ,  $y_1 + s_2 y_2$ ,  $z_1 + s_3 z_2$ , and  $w_1 + s_4 w_2$  to approach zero. In this case, the output response of the second system is given by

$$\begin{aligned} x_2(t) &= -\frac{x_1(t)}{s_1(t)}, \\ y_2(t) &= -\frac{y_1(t)}{s_2(t)}, \end{aligned}$$

$$z_2(t) = -\frac{z_1(t)}{s_3(t)},$$

$$w_2(t) = -\frac{w_1(t)}{s_4(t)}.$$

(8)

Then, if  $s_1 = s_2 = s_3 = s_4 = -1$ , this will be the conventional synchronization, and if  $s_1 = s_2 = s_3 = s_4 = 1$ , this will be the antisynchronization as will be discussed in the next subsection. Moreover, the scaling functions  $s_i(t)$ ,  $i = 1, 2, 3, 4$ , can have different values and time-dependent functions are discussed in the next subsections.

**3.1. Nonlinear Antisynchronization of Two Identical Fractional-Order Chaotic Chua's Circuit Systems** ( $s_i = 1$ ,  $i = 1, 2, 3, 4$ ). In this subsection we observe the antisynchronization behavior in two identical fractional-order chaotic Chua's circuit systems via nonlinear control. The drive (master) and slave (response) systems are described, respectively, by the following equations. However, the initial condition on the drive system is different from that of the response system:

$$D^\alpha x_1(t) = a_1(y_1 - f(w_1)x_1), \quad (9a)$$

$$D^\beta y_1(t) = z_1 - x_1, \quad (9b)$$

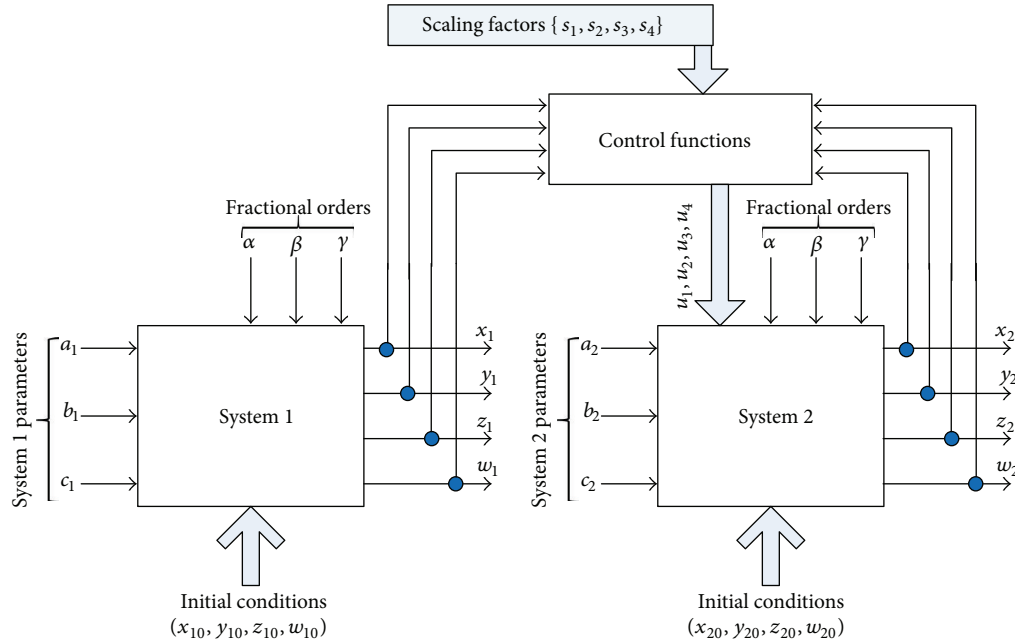


FIGURE 2: The proposed block diagram.

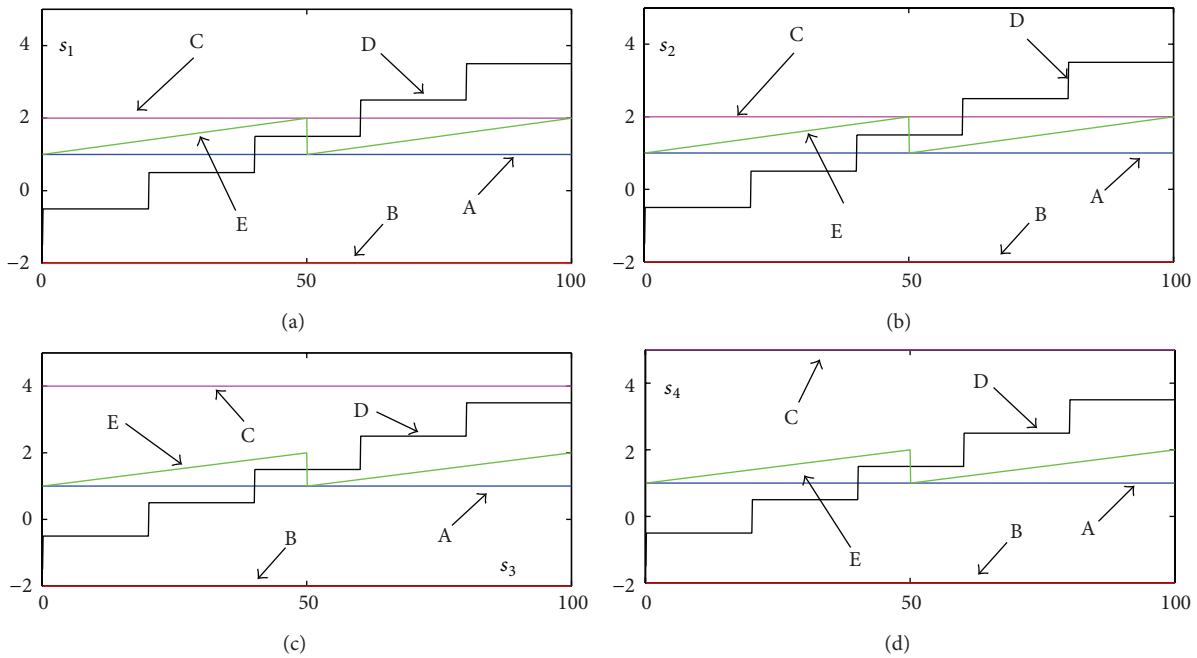


FIGURE 3: The five different cases of the parameters  $s_1, s_2, s_3$ , and  $s_4$  as function of time where Case A;  $\{s_1, s_2, s_3, s_4\} = \{1, 1, 1, 1\}$  Case B;  $\{s_1, s_2, s_3, s_4\} = \{-2, -2, -2, -2\}$  Case C;  $\{s_1, s_2, s_3, s_4\} = \{2, 3, 4, 5\}$  Case D;  $s_1 = s_2 = s_3 = s_4 = -0.5 + \text{integer part of } (t/20)$ , Case E;  $s_1 = s_2 = s_3 = s_4 = 1 + (\text{fraction part of } (t/50))/50$ .

$$D^\gamma z_1(t) = -b_1 y_1 + c_1 z_1, \quad (9c)$$

$$Dw_1(t) = x_1, \quad (9d)$$

$$D^\gamma z_2(t) = -b_2 y_2 + c_2 z_2 + u_3, \quad (10c)$$

$$Dw_2(t) = x_2 + u_4, \quad (10d)$$

$$D^\alpha x_2(t) = a_2 (y_2 - f(w_2) x_2) + u_1, \quad (10a)$$

$$D^\beta y_2(t) = z_2 - x_2 + u_2, \quad (10b)$$

where the control function  $u = [u_1; u_2; u_3; u_4]^T = 0$ . Our goal is to determine the control function to make the first derivative of  $V(e)$ , that is,  $V(e) < 0$ . From (9a), (9b), (9c),

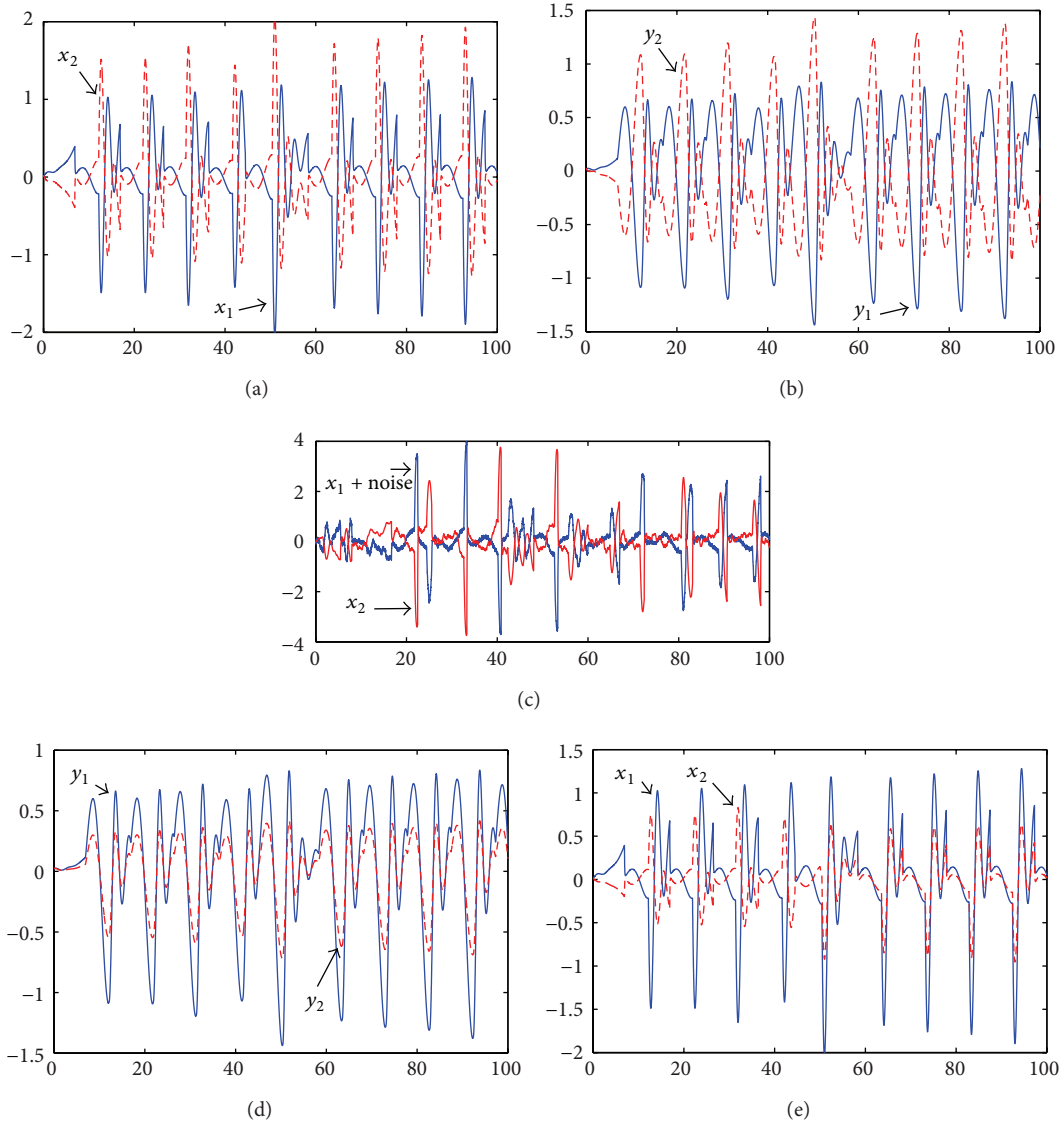


FIGURE 4: The general synchronization of (a), (b) the  $x$  and  $y$  responses when  $\{\alpha, \beta, \gamma, a_1, b_1, c_1, a_2, b_2, c_2\} = \{0.96, 0.96, 0.96, 4, 1, 0.65, 4, 1, 0.65\}$  for Case A, (c) the  $x$  response under the same condition with additive noise with amplitude 0.1, (d) the response when  $\{\alpha, \beta, \gamma, a_1, b_1, c_1, a_2, b_2, c_2\} = \{0.96, 0.96, 0.96, 4, 1, 0.65, 4, 1, 0.65\}$  for Case B, and (e) Case C.

and (9d) to (10a), (10b), (10c), and (10d), the error equations when the system parameters  $\{a_1, b_1, c_1\} = \{a_2, b_2, c_2\} = \{a, b, c\}$  are given as follows:

$$D^\alpha e_x = ae_y - a(f(w_1)x_1 - f(w_2)x_2) + u_1, \quad (11a)$$

$$D^\beta e_y = e_z - e_x + u_2, \quad (11b)$$

$$D^\gamma e_z = -be_y + ce_z + u_3, \quad (11c)$$

$$De_w = e_x + u_4, \quad (11d)$$

where  $e_x = x_2 + x_1$ ,  $e_y = y_2 + y_1$ ,  $e_z = z_2 + z_1$ ,  $e_w = w_2 + w_1$ . In order to determine the controller, let

$$u_1 = u_{1a} + u_{1b}, \quad u_{1b} = -a(f(w_1)x_1 + f(w_2)x_2). \quad (12)$$

Then we rewrite system (11a), (11b), (11c), and (11d) in the following form:

$$D^\alpha e_x = ae_y + u_{1b}, \quad (13a)$$

$$D^\beta e_y = e_z - e_x + u_2, \quad (13b)$$

$$D^\gamma e_z = -be_y + ce_z + u_3, \quad (13c)$$

$$De_w = e_x + u_4. \quad (13d)$$

Based on the Lyapunov stability theory, when the controller satisfies the assumption  $V(e) = 0.5e^T e$ , a positive definite function, the first derivative of  $V(e)$ ,  $V(e) < 0$ , and the antisynchronization of two identical Chua's circuit systems

from different initial conditions is achieved, we choose  $u$  as follows:

$$u_{1b} = -e_x - ae_y, \quad (14a)$$

$$u_2 = -e_z + e_x - e_y, \quad (14b)$$

$$u_3 = -2ce_z + be_y, \quad (14c)$$

$$u_4 = -e_x - e_u. \quad (14d)$$

**Theorem 1.** *The nonlinear controller achieves global anti-synchronization between two identical Chua's circuit systems master (9a), (9b), (9c), and (9d) and slave (10a), (10b), (10c), and (10d).*

*Proof.* Take a Lyapunov function for (13a), (13b), (13c), and (13d) into consideration as

$$V(e) = 0.5e^T e. \quad (15)$$

We then get the first derivative of  $V(e)$ :

$$\begin{aligned} \dot{V} = & e_x (ae_y + u_{1b}) + e_y (e_z - e_x + u_2) \\ & + e_z (-be_y + ce_z + u_3) \end{aligned}$$

$$+ e_w (e_x + u_4), \quad (16a)$$

$$\dot{V} = -e_x^2 - e_y^2 - bce_z^2 - e_w^2, \quad (16b)$$

so  $\dot{V}(e) < 0$  is satisfied. Since  $\dot{V}(e)$  is a negative-definite function [39], the error states tend to zero at steady state. Therefore, the states of controlled response system and drive system are globally antisynchronized asymptotically.  $\square$

**3.2. Generalized Projective Synchronization of Two Identical Chua's Circuits.** In this subsection we study the synchronization between two identical fractional-order chaotic Chua's circuits based on the generalized projective synchronization. The unknown terms  $u_1, u_2, u_3$ , and  $u_4$  in (11a), (11b), (11c), and (11d) are active control functions to be determined. Define the error functions as

$$\begin{pmatrix} e_x(t) \\ e_y(t) \\ e_z(t) \\ e_w(t) \end{pmatrix} = \begin{pmatrix} x_1(t) + s_1(t)x_2(t) \\ y_1(t) + s_2(t)y_2(t) \\ z_1(t) + s_3(t)z_2(t) \\ w_1(t) + s_4(t)w_2(t) \end{pmatrix}. \quad (17)$$

Then by similar procedure, the control functions are given by

$$\begin{pmatrix} u_1(t) \\ u_2(t) \\ u_3(t) \\ u_4(t) \end{pmatrix} = \begin{pmatrix} \frac{(a_1 f(w_1(t)) - k_x)x_1(t) - a_1 y_1(t)}{s_1(t)} + (a_2 f(w_2(t)) - k_x)x_2(t) - a_2 y_2(t) \\ \frac{x_1(t) - z_1(t) - k_y y_1(t)}{s_2(t)} + x_2(t) - z_2(t) - k_y y_2(t) \\ \frac{b_1 y_1(t) - c_1 z_1(t) - k_z z_1(t)}{s_3(t)} + b_2 y_2(t) - c_2 z_2(t) - k_z z_2(t) \\ \frac{-x_1(t) - k_w w_1(t)}{s_4(t)} + -x_2(t) - k_w w_2(t) \end{pmatrix}. \quad (18a)$$

Then

$$\begin{pmatrix} D^\alpha e_x \\ D^\beta e_y \\ D^\gamma e_z \\ D e_w \end{pmatrix} = \begin{pmatrix} -k_x & 0 & 0 & 0 \\ 0 & -k_y & 0 & 0 \\ 0 & 0 & -k_z & 0 \\ 0 & 0 & 0 & -k_w \end{pmatrix} \begin{pmatrix} e_x \\ e_y \\ e_z \\ e_w \end{pmatrix} \quad (18b)$$

which are decaying functions as the values of  $k_x, k_y, k_z$ , and  $k_w$  are positive.

#### 4. Numerical Results

Nonstandard finite difference method with  $\phi(h) = 1 - e^{-h}$  is used to solve the systems of differential equations. In addition, a time step size 0.01 is employed. We select the parameters of the master system of Chua's circuit system as

$a_1 = 4, b_1 = 1, c_1 = 0.65, m_1 = 0.2$ , and  $m_2 = 5$ , so these systems exhibit chaotic behavior with the following initial conditions:

$$\begin{pmatrix} x_1(0) \\ y_1(0) \\ z_1(0) \\ w_1(0) \end{pmatrix} = \begin{pmatrix} 0.01 \\ 0.02 \\ 0.01 \\ 0.05 \end{pmatrix}, \quad (19)$$

$$\begin{pmatrix} x_2(0) \\ y_2(0) \\ z_2(0) \\ w_2(0) \end{pmatrix} = \begin{pmatrix} 0.02 \\ 0.03 \\ 0.02 \\ 0.06 \end{pmatrix}.$$

To validate the proposed technique, five different cases of the scaling parameters  $s_1(t), s_2(t), s_3(t)$ , and  $s_4(t)$  are discussed as shown in Figure 3 and we have the following.

(i) *Case A* ( $\{s_1, s_2, s_3, s_4\} = \{1, 1, 1, 1\}$ ). In this case the scaling parameters are positive ones; then the output responses of system 2 are the antisynchronization of the system 1 output, that is,  $x_2 = -x_1$  and the same for other outputs



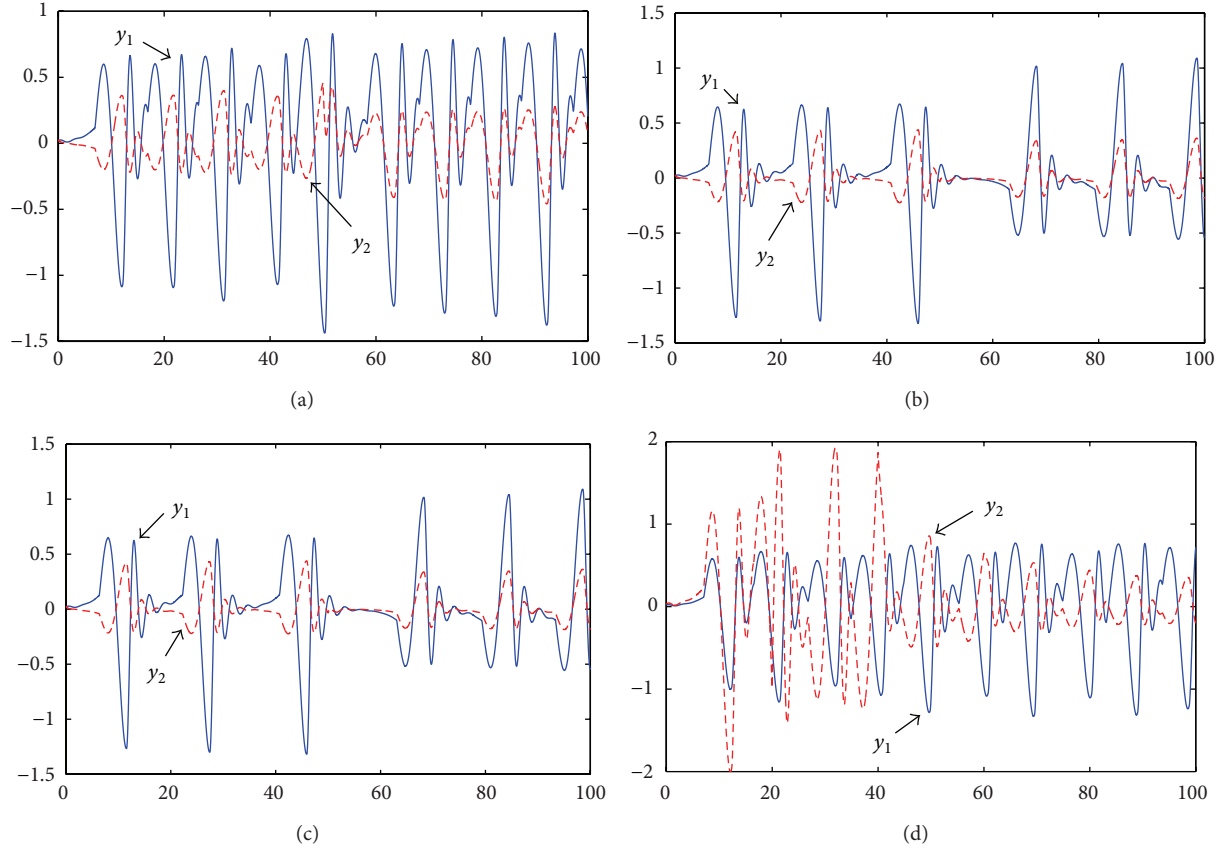


FIGURE 5: The  $y$  response when for Case D when (a)  $\{\alpha, \beta, \gamma, a_1, b_1, c_1, a_2, b_2, c_2\} = \{0.96, 0.96, 0.96, 4, 1, 0.65, 4, 1, 0.65\}$ , (b)  $\{\alpha, \beta, \gamma, a_1, b_1, c_1, a_2, b_2, c_2\} = \{0.9, 0.95, 1, 4, 1, 0.65, 4, 1, 0.65\}$ , (c)  $\{\alpha, \beta, \gamma, a_1, b_1, c_1, a_2, b_2, c_2\} = \{0.9, 0.95, 1, 4, 1, 0.65, 4.5, 1.2, 0.55\}$ , and (d)  $\{\alpha, \beta, \gamma, a_1, b_1, c_1, a_2, b_2, c_2\} = \{0.95, 0.95, 0.95, 4, 1, 0.65, 4, 1, 0.65\}$ .

(see Figures 4(a) and 4(b)). Moreover, when an additive random noise is added to both the  $X_1$  and  $Y_1$  with amplitude 0.1 under the same conditions, the output response tries to follow the changes as shown in Figure 4(c).

(ii) *Case B* ( $\{s_1, s_2, s_3, s_4\} = \{-2, -2, -2, -2\}$ ). In this case the scaling parameters are equal and negative; then the output responses of system 2 are the half-synchronization of the system 1 output, that is,  $x_2 = 0.5 x_1$  and the same for other outputs (see Figure 4(d)).

(iii) *Case C* ( $\{s_1, s_2, s_3, s_4\} = \{2, 3, 4, 5\}$ ). In this case the scaling parameters are different constants and positive; then the output responses of system 2 have different antisynchronization scale than system 1 output, that is,  $x_2 = -0.5 x_1$ ,  $y_2 = -y_1/3$ ,  $z_2 = -z_1/4$ , and  $w_2 = -w_1/5$  (see Figure 4(e)).

(iv) *Case D* ( $s_1 = s_2 = s_3 = s_4 = -0.5 + \text{integer part of } (t/20)$ ). In this case the scaling parameters are time dependent (staircase) as steps (every 20 seconds); then the output responses of system 2 will start with double synchronization in the first 20 seconds and then double antisynchronization in the following 20 seconds, and the scale factor increases with time every 20 seconds (see Figure 5).

(v) *Case E* ( $s_1 = s_2 = s_3 = s_4 = 1 + (\text{fraction part of } (t/50))/50$ ). In this case the scaling parameters are time dependent as they ramp up to 50 seconds and then reset and increase again. Since it is always positive, then the output response will be the antisynchronization of system 1 with a different scale (see Figure 6).

Figure 5 shows the proposed technique under different orders and different system parameters where the output will follow the expected response; however the transient time until the synchronization happens may be increased. Figures 5(b) and 5(c) illustrate the response with different fractional orders where  $\alpha = 0.9$ ,  $\beta = 0.95$ , and  $\gamma = 1.0$ , and Figure 5(c) shows the responses for different fractional orders and also system parameters  $\{\alpha, \beta, \gamma, a_1, b_1, c_1, a_2, b_2, c_2\} = \{0.9, 0.95, 1, 4, 1, 0.65, 4.5, 1.2, 0.55\}$ . Moreover, Figure 5(d) shows the system responses for equal fractional orders and different system parameters only. Therefore, many cases have been discussed when the synchronization parameters are changed by steps showing great matching with the expected results. Figure 6 illustrates the projections and system responses when the synchronization parameters change gradually and linearly resulting in a sawtooth waveform (Case E). It is clear from the previous responses for different system parameters, fractional orders, and time-independent

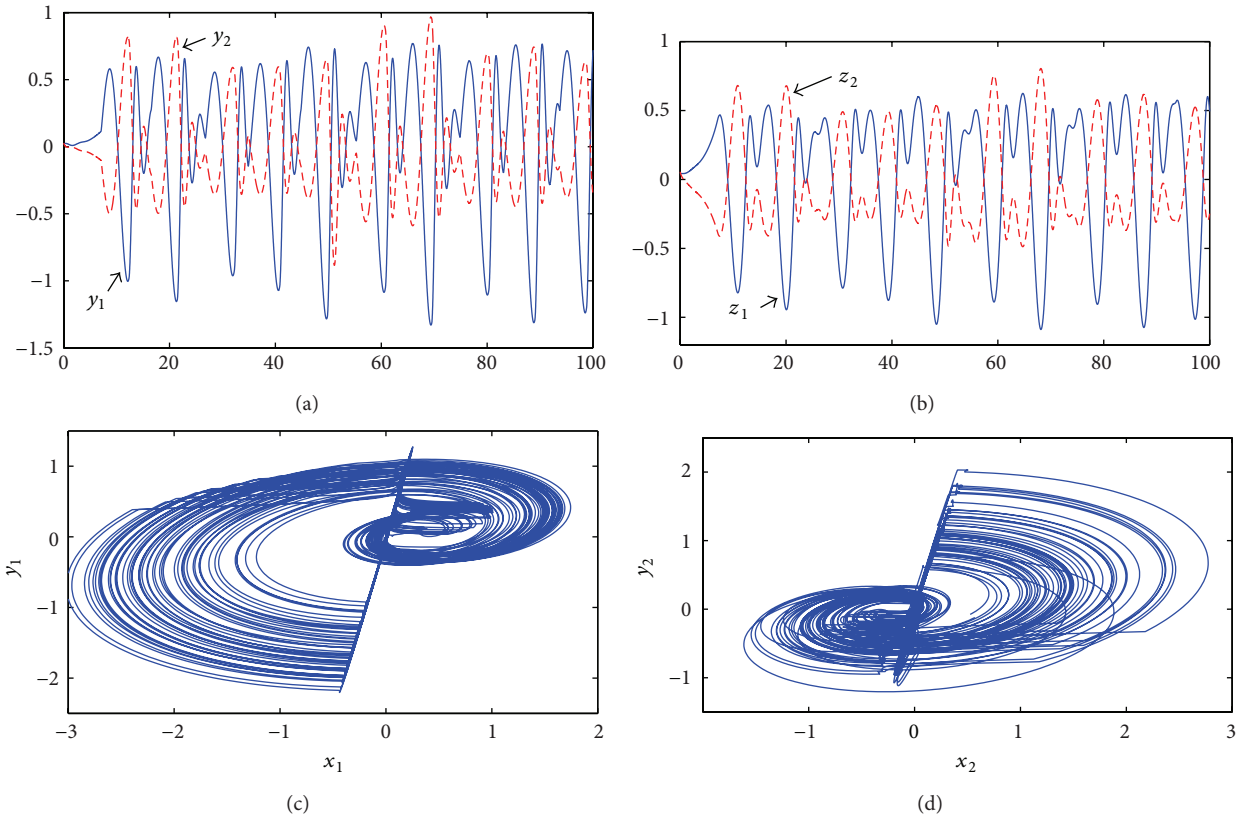


FIGURE 6: ((a), (b)) the  $x_1$ - $y_1$  and  $x_2$ - $y_2$  projections, and ((c), (d)) the  $x$ ,  $y$ , and  $z$  responses when  $\{\alpha, \beta, \gamma, a_1, b_1, c_1, a_2, b_2, c_2\} = \{0.95, 0.95, 0.95, 4, 1, 0.65, 4, 1, 0.65\}$  for Case E.

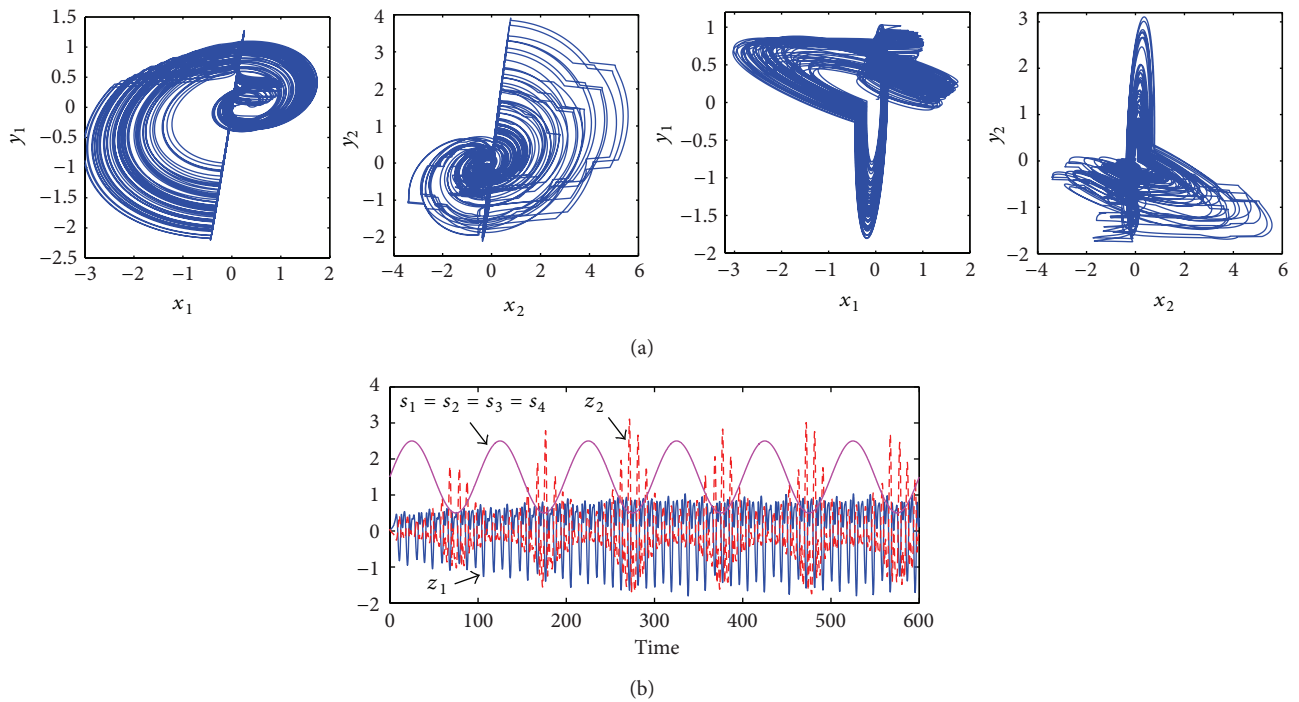


FIGURE 7: The projection and responses for the amplitude modulation when  $s_1(t) = s_2(t) = s_3(t) = s_4(t) = 1.5 + \sin(0.02\pi t)$ .



and time-dependent synchronization parameters that the proposed method has many advantages and can be used for the synchronization of any two chaotic systems. There are many recent research articles which discuss the importance of communication techniques using chaotic signals [40, 41]. In the amplitude modulation, the amplitude of the output signal should be a function of the input signal. In Figure 7, we assumed that the information data  $s_1(t) = s_2(t) = s_3(t) = s_4(t) = 1.5 + \sin(0.02\pi t)$ . Therefore, the output will be different from system 1 output as shown from the strange attractors shown in Figure 7(a). The time waveform of the scaling functions,  $z_1(t)$ , and  $z_2(t)$ , is shown in Figure 7(b) where the modulation is clear. The demodulation can be done similarly by reversing the operation.

## 5. Conclusions

This paper discussed the concept of a general time-dependent synchronization scheme based on a nonlinear controller and then applied this technique on the fractional-order Chua's circuit with memristor. This nonlinear controller is based on the control theory and Lyapunov stability theory to achieve the required synchronization. Many examples including anti-synchronization, synchronization, and both (as in Case D) between two identical fractional-order Chua's circuits with same/different fractional orders and same/different system parameters are discussed using numerical simulations by the nonstandard finite method. This technique can be repeated for other chaotic systems in a similar way to achieve good results.

## Conflict of Interests

The authors declare that there is no conflict of interests regarding the publication of this paper.

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